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Short communication

# Low-loss and low-temperature firable Li<sub>2</sub>Mg<sub>3</sub>SnO<sub>6</sub>-Ba<sub>3</sub>(VO<sub>4</sub>)<sub>2</sub> microwave dielectric ceramics for LTCC applications



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ARTICLE INFO	A B S T R A C T				
Keywords:	A new low-loss and low-temperature fired $(1 - x)Li_2Mg_3SnO_6-xBa_3(VO_4)_2-3$ wt% LiF $((1 - x)L_2MS-xBV-2)$				
Microwave dielectrics Ceramics Composite Co-sintering LTCC	0.03LiF) ceramic was prepared via a conventional solid-state route. The results indicate that L <sub>2</sub> MS and BV phases can stably convist in the composite up to at least 900 °C. The appearance of a secondary phase Li MaSn-O <sub>2</sub> at				
	temperatures lower than 800 $^{\circ}$ C was ascribed to the low-temperature decomposition of L <sub>2</sub> MS, irrespective of the existence of BV or LiF. Microwave dielectric properties of L <sub>2</sub> MS-BV composites generally displayed a nearly				
	linear relation with x and obeyed a well-known mixing rule. With the help of 3 wt% LiF, the $x = 0.37$ sample				
	sintered only at 850 °C for 6 h exhibited excellent microwave dielectric properties of $\varepsilon_r = 12.8$ , $Q \times f = 101.705$ GHz (@ 9.64 GHz) and near-zero $\tau_c$ of $-2.9$ ppm/°C. The good chemical compatibility with Ag further				
	indicates that the $0.63L_2MS - 0.37BV-0.03LiF$ composite ceramic would be a promising dielectric material for				

low temperature co-fired ceramic applications.

# 1. Introduction

Low-temperature co-fired ceramic (LTCC) technology has become crucial for modern wireless communication system, which requires dielectric materials to own low sintering temperatures, excellent chemical compatibility with Ag electrode, near-zero temperature coefficient of resonant frequency ( $\tau_f$ ), high quality factor ( $Q \times f > 5000$  GHz) and appropriate dielectric constant ( $\varepsilon_r$ ) [1,2]. A lot of research work has been focused on developing new low-loss LTCC materials with excellent performances [3,4].

Rock salt-structured  $Li_2Mg_3BO_6$  ( $L_2MB$ , B = Ti, Sn, Zr) ceramic system has attracted extensive attention in recent years owing to its ultra-low loss [5–7].  $L_2MB$  (B = Ti, Sn, Zr) ceramics sintered at 1280, 1360 and 1380 °C possessed excellent microwave dielectric properties of  $\varepsilon_r$  = 15.2, 8.8 and 12.6,  $Q \times f$  = 152,000, 123,000 and 86,000 GHz, and  $\tau_f = -39$ , -32 and -36 ppm/°C, respectively [5]. However, the porous microstructure and secondary phases caused by lithium evaporation have significantly deteriorated their microwave dielectric properties. The pure-phase L<sub>2</sub>MB ceramics could be prepared by means of atmosphere controlled sintering through burying the sample pellets in sacrificial powder of the same composition. As a result, greatly enhanced  $Q \times f$  values of 110,000–300,000 GHz were attained in wellsintered ceramics [6,7]. The outstanding microwave dielectric properties have highlighted their enormous potentials, but the high sintering temperature and large  $\tau_f$  values have hindered their practical

applications. A near-zero  $\tau_f$  value was reported in Li<sub>2</sub>Mg<sub>3</sub>TiO<sub>6</sub> ceramics with the addition of  $Ca_{0.8}Sr_{0.2}TiO_3$  or the substitution of 12% Ca for Mg, resulting from the secondary phase with an opposite-sign  $\tau_f$  value [8-10]. However, CaTiO<sub>3</sub> or Ca<sub>0.8</sub>Sr<sub>0.2</sub>TiO<sub>3</sub> inherently has a high sintering temperature (> 1350 °C) and a high loss (< 5000 GHz) [11], which would significantly sacrifice the  $Q \times f$  value of the matrix composition for achieving a near-zero  $\tau_f$  value. By comparison,  $Ba_3(VO_4)_2$  (BV) is a superior  $\tau_f$  compensator due to its large positive  $\tau_f$ value (  $\sim~+52$  ppm/°C) and especially good dielectric performances ( $\varepsilon_r$ = 14 and  $Q \times f$  = 42,000 GHz) as well as relatively low temperatures (~ 1100 °C) [12]. It has been used in many composite ceramics, for instance, BV-LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub>, BV-BaWO<sub>4</sub>, BV-Zn<sub>2-x</sub>SiO<sub>4-x</sub>, BV-Mg<sub>2</sub>SiO<sub>4</sub>, BV-Li<sub>3</sub>(Mg<sub>0.92</sub>Zn<sub>0.08</sub>)<sub>2</sub>NbO<sub>6</sub> and etc. [13-17], in which the sintering temperature could be lowered obviously in addition to satisfactory microwave dielectric properties.

LiF was often used to improve the sintering behavior of Li-based dielectric ceramics and successfully reduced the sintering temperature below 950 °C [18-21]. The 3 wt% LiF aided Li2Mg3SnO6 (L2MS) ceramics were reported to have excellent microwave dielectric properties of  $\varepsilon_r = 11.6, Q \times f = 133,000 \text{ GHz}$  and  $\tau_f = -37 \text{ ppm/°C}$  as sintered only at 875 °C [19]. In this study,  $(1 - x)L_2MS-xBV-3$  wt% LiF (x in volume fraction) ceramics were investigated for the purpose to achieve a desirable LTCC microwave dielectric ceramic with a low loss and a near-zero  $\tau_{f_1}$  in which LiF played a crucial role in both further reducing the sintering temperature, and suppressing the possible reaction or

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inter-diffusion between  $L_2\text{MS}$  and BV due to the reduced sintering temperature.

## 2. Experimental procedure

L<sub>2</sub>MS and BV powders were synthesized by means of a conventional mixed-oxide route using high-purity (> 99%) raw powders of  $Li_2CO_3$ , MgO, SnO<sub>2</sub>, BaCO<sub>3</sub>, LiF (Sinopharm Chemical Reagent Co., Ltd., Shanghai, China) and V<sub>2</sub>O<sub>5</sub> (Shandong Xiya Reagent Chemistry Co., Ltd, Linshu, China) according to their respective stoichiometric proportions. Powder mixtures were ball-milled for 8 h in alcohol. After drving, L<sub>2</sub>MS and BV powders were calcined at 1100 °C and 800 °C for 8 h. respectively. Afterwards, the pre-calcined powders were weighed according to the prescribed formula of  $(1 - x)L_2MS-xBV$  (x = 0.20-0.55 in volume fraction) together with 3 wt% LiF as a sintering aid. After being re-milled for 6 h, the fine powders were granulated with 5 wt% PVA as a binder and then subsequently pressed into cylinders with dimensions of 10 mm in diameter and 5-6 mm in height. These samples were sintered in air in the temperature range from 750 °C to 900 °C for 6 h. For the chemical compatibility test, the above-mentioned powder mixture was co-fired with 30 wt% Ag powder at 850 °C for 6 h. To prevent lithium evaporation during sintering, green pellets were buried in the powder of the same composition.

The bulk densities of the sintered ceramics were measured using the Archimedes method. The crystalline phases were identified by an X-ray diffractometer (XRD; D/Max2500 V, Rigaku, Tokyo, Japan). The microstructure of the sintered samples was observed using a field-emission scanning electron microscope (FE-SEM; SU8020, JEOL, Tokyo, Japan) equipped with an energy-dispersive X-ray spectroscope (EDS). Microwave dielectric properties were measured by the Hakki-Coleman method and the TE<sub>01δ</sub>-shield cavity method with a network analyzer (N5230C; Agilent, Palo Alto, CA) [22] in the frequency range of 9–13 GHz. The  $\tau_f$  value of the samples was measured in the temperature range from 20 °C to 80 °C.

# 3. Results and discussion

The normalized XRD patterns of a few powder samples are displayed in Fig. 1. As shown in Fig. 1(a), all diffraction peaks of the ascalcined L2MS and BV powders could be indexed to the standard patterns of L<sub>2</sub>MS (PDF #39-0932) and BV (PDF #29-0211), respectively, indicating that pure L2MS and BV have been successfully prepared. The former exhibits a cubic rock-salt structure with Fm-3m space group while the latter belongs to a rhombohedral structure with R-3m space group. The big difference in their crystal structures would guarantee the coexistence of BV and L<sub>2</sub>MS phases in the co-fired sample. As indicated in Fig. 1(b), only L<sub>2</sub>MS and BV phases were observed in the 0.63L<sub>2</sub>MS-0.37BV-0.03LiF ceramic sintered at 850 °C and 900 °C, indicating that there is no chemical reaction among BV, L2MS and LiF. However, when sintering temperature was lower than 850 °C, an additional phase Li<sub>4</sub>MgSn<sub>2</sub>O<sub>7</sub> (L<sub>4</sub>MS, PDF #37-1164) appeared in the sample and its concentration slightly increased with decreasing sintering temperature from 775 °C to 750 °C. In order to illustrate the origin of the secondary phase L₄MS, the XRD patterns of L₂MS, L₂MS-0.03LiF and BV-0.03LiF ceramics sintered at 800 °C for 6 h were used for comparison. No any secondary phase can be observed in the BV-0.03LiF sample sintered at 800 °C. Moreover, the same phase composition was observed in both L2MS and L2MS-0.03LiF samples as they were sintered at 800 °C. Apart from the dominant phase L<sub>2</sub>MS, both samples contained the secondary phase L<sub>4</sub>MS. In combination with the XRD result of 0.63L<sub>2</sub>MS-0.37BV-0.03LiF sintered at 850 °C or 900 °C, one can believe that the appeared secondary phase L4MS should come from the low-temperature decomposition of L<sub>2</sub>MS. As manifested by the phase diagram of Li<sub>2</sub>SnO<sub>3</sub>-MgO [23], L<sub>4</sub>MS exists at lower temperatures and tends to transform into the MgO-structured solid solution (i.e. L2MS in this work) as sintering temperature increases above a certain value, which depends on the



Fig. 1. XRD patterns of (a) BV and  $L_2MS$  samples as calcined and (b) different samples sintered at varying temperatures as indicated compared with the standard patterns of  $L_2MS$ , BV and  $L_4MS$ .

molar ratio of  $Li_2SnO_3$  and MgO. That is the reason why a slightly increased amount of  $L_4MS$  could be observed as sintering temperature was reduced down to 750 °C.

Fig. 2 shows SEM images of the x = 0.37 sample sintered at 850 °C for 6 h. The secondary electron image shown in Fig. 2(a) indicates a dense microstructure with closely packed polygonal grains (~  $2 \mu m$  in average). It is almost impossible to distinguish the grains between L<sub>2</sub>MS and BV phases from the grain morphology. However, the coexisting two phases can be clearly identified from the corresponding backscattered electron image shown in Fig. 2(b), where there were two kinds of grains with different gray levels owing to the mass difference of the elements in the respective grain. The EDS result listed in Table 1 shows that the dark grains (marked as spectrum 1 in Fig. 2(b)) mainly contained Mg, Sn, O elements with an approximate molar ratio of Mg:Sn:O = 3:1:6 (lithium is too light to be precisely detected by EDS), which approximately corresponds to the composition of L<sub>2</sub>MS. The light grains (marked as spectrum 2 in Fig. 2(b)) were dominantly composed of Ba, V, and O elements with a Ba:V ratio of  $\sim$  3:2, suggesting that these grains belong to the BV phase. The above analysis further illustrates a composite structure of the x = 0.37 sample consisting of L<sub>2</sub>MS and BV phases, which agreed well with the XRD results in Fig. 1. In addition, it can be also seen from Table 1 that a few amount of  $Ba^{2+}$  and  $V^{5+}$  were detected in the  $L_2MS$  grain, meanwhile some Mg<sup>2+</sup> and Sn<sup>4+</sup> appeared in the BV grain, indicating the existence of the ionic inter-diffusion between the two phases during co-sintering. The similar phenomena were also observed in the BV-LiMg<sub>0.9</sub>Zn<sub>0.1</sub>PO<sub>4</sub> and BV-Li<sub>3</sub>(Mg<sub>0.92</sub>Zn<sub>0.08</sub>)<sub>2</sub>NbO<sub>6</sub> composite ceramics [13,17].

Relative density and microwave dielectric properties of (1 - x) L<sub>2</sub>MS-xBV-0.03LiF ceramics sintered at different temperatures are shown in Fig. 3. With increasing sintering temperature, the relative density of all specimens increased to the maximum values approximately at 775 °C, and then remained almost constant (> 95%) within the studied temperature range ( $\leq$  900 °C). This result indicates that the



Table 1 EDS results of the x = 0.37 sample as shown in Fig. 2(b).

Points	Element		Total (%)			
	Mg	Sn	Ва	V	0	
1	29.5 10 1	12.1 3.6	0.8 30.1	0.4 18.2	57.2 38.0	100.0 100.0

addition of 3 wt% LiF effectively promoted the densification of (1 - x) L<sub>2</sub>MS-xBV ceramics and made them well densified within a relatively low sintering temperature [19]. The variation of  $\varepsilon_r$  and  $Q \times f$  values with sintering temperature showed a similar trend to that of the relative density, indicating that both  $\varepsilon_r$  and  $Q \times f$  values mainly depended on the sample density in this work. The secondary phase formed below 850 °C did not bring obvious effects on the dielectric properties of the matrix, implying that L<sub>4</sub>MS probably owns a similar dielectric performance with L<sub>2</sub>MS. As the sintering temperature was higher than 775 °C,

 $\varepsilon_r$  and  $Q \times f$  generally kept nearly constant for samples with a certain x value. However, for samples with different x values, their dielectric properties were found to be strongly dependent on the relative content of L<sub>2</sub>MS and BV, as shown in Fig. 3(d). Fig. 3(d) indicates that ln  $\varepsilon_r$ , ( $Q \times f$ )<sup>-1</sup>, and  $\tau_f$  values displayed a nearly linear variation as a function of x, which is in good agreement with a well-known empirical model for multiphase ceramics described as follows [24,25]:

$$\ln \varepsilon_r = V_1 \ln \varepsilon_{r1} + V_2 \ln \varepsilon_{r2} \tag{1}$$

$$(Q \times f)^{-1} = V_1 (Q \times f)_1^{-1} + V_2 (Q \times f)_2^{-1}$$
<sup>(2)</sup>

$$\tau_f = V_1 \tau_{f1} + V_2 \tau_{f2} \tag{3}$$

where  $V_1$  and  $V_2$  stand for the volume fraction of each phase. A slight deviation between the experimental and calculated ln  $\varepsilon_r$  and  $(Q \times f)^{-1}$  values could be clearly observed, as also found in other studies [15,25]. One reason might be ascribed to the fact that the distribution of two phases is not perfectly uniform in the sintered ceramic body. Moreover, the microwave dielectric properties of these two phases in the



Fig. 3. (a) Relative density, (b)  $e_r$  and (c)  $Q \times f$  values of  $(1 - x)L_2$ MS-xBV-0.03LiF ceramics sintered at different temperatures, and (d) the measured and calculated dielectric properties with changing the volume fraction (x) of BV for samples sintered at 850 °C for 6 h.

Fig. 2. (a) Secondary electron image and (b) backscattered electron image on the polished and thermally etched surface of the x = 0.37 sample sintered at 850 °C for 6 h.

#### Table 2

A comparison of microwave dielectric properties among a few LTCC ceramics with rock salt structure.

Compounds	S.T. (°C)	£ <sub>r</sub>	$Q \times f(GHz)$	$\tau_f (\text{ppm/°C})$	Ref.
$\begin{array}{l} 0.8 Li_2 Mg_3 TiO_6 - 0.2 Ca_{0.8} Sr_{0.2} TiO_3 \ -4 \ wt\% \ LiF \\ 0.7 Li_3 (Mg_{0.92} Zn_{0.08})_2 NbO_6 - 0.3 BV \\ Li_2 Mg TiO_4 - 10 \ wt\% LiF \\ -12 \ wt\% \ Ca_{0.8} Sr_{0.2} TiO_3 \\ Li_2 SnO_3 - 8 \ wt\% \ MgO - 2 \ wt\% \ LiF \end{array}$	800 950 900 880	18.8 16.3 18 14.7	48,200 50,084 34,800 78,400	0.3 1.5 4 -0.9	[8] [17] [20] [21]
0.63L <sub>2</sub> MS-0.37BV-0.03LiF	850	12.8	101,705	-2.9	This work

S.T.: sintering temperature; Ref.: references.



Fig. 4. (a) Backscattered electron image and (b) XRD pattern of the x=0.37 sample co-fired with Ag at 850  $^\circ C$  for 6 h.

composite ceramic might be different from those in their respective monophasic ceramics owing to the ionic inter-diffusion during sintering [26], as discussed above. By contrast, a nearly linear curve was observed for both experimental and calculated  $\tau_f$  values with increasing x, apart from their close values. This may be due to the fact  $\tau_f$  is more sensitive to the intrinsic structure of each phase, which was nearly unchanged before and after sintering. Nevertheless, excellent microwave dielectric properties of  $\varepsilon_r = 12.8$ ,  $Q \times f = 101,705$  GHz (@ 9.64 GHz) and  $\tau_f = -2.9$  ppm/°C were achieved in the x = 0.37 ceramic sintered at 850 °C for 6 h. A comparison of microwave dielectric properties for a few LTCC ceramics with similar structures was made, as shown in Table 2. Among these ceramics, it is easy to find that high  $Q \times f$  values and low sintering temperatures in current 0.63L<sub>2</sub>MS-0.37BV-0.03LiF composite ceramic made it have relatively large potentials against others.

For the chemical compatibility test, the composite ceramic powder was co-fired with 30 wt% Ag powder at 850 °C for 6 h. As shown in Fig. 4(a), the backscattered electron image clearly indicated that silver particles can stably exist in the  $0.63L_2MS-0.37BV-0.03LiF$  ceramic after sintering. A clear interface between the ceramic particles and silver particles suggested no chemical reaction between them. This can be further confirmed by the corresponding XRD result shown in Fig. 4(b). All diffraction peaks of the co-fired sample can be well indexed to the L<sub>2</sub>MS, BV, and Ag. As a result, the composite ceramic reported in current study possesses a good chemical compatibility with Ag electrodes in addition to excellent microwave dielectric properties, being expected as a promising candidate material for LTCC applications.

### 4. Conclusions

The phase composition, microstructure and microwave dielectric properties of the  $(1 - x)L_2MS-xBV-0.03LiF$  composite ceramics were systematically investigated, in which LiF and BV acted as a sintering aid and a  $\tau_f$  compensator, respectively. The XRD results reveal that L<sub>2</sub>MS and BV phases stably coexisted in the sintered ceramics at the sintering temperature up to at least 900 °C. At temperatures lower than 800 °C, the appearance of a secondary phase L4MS stemmed from the lowtemperature decomposition of L2MS, irrespective of the existence of BV and LiF, through which a low-temperature sintering and a near-zero  $\tau_f$ can be obtained by adjusting the relative content of BV and L2MS according to a well-known mixing rule. Excellent microwave dielectric properties of  $\varepsilon_r$  = 12.8,  $Q \times f$  = 101,705 GHz (@ 9.64 GHz) and  $\tau_f$  = -2.9 ppm/°C were achieved in the x = 0.37 sample sintered at 850 °C for 6 h. Furthermore, the 0.63L2MS-0.37BV-0.03LiF composite ceramic has a good chemical compatibility with Ag, suggesting its great potential for LTCC applications.

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